

Toward a Nonlinear Acoustic Analogy: Turbulence as a Source of Sound and Nonlinear Propagation

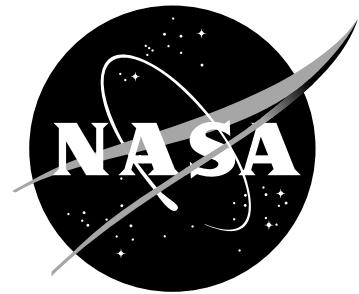
Steven A. E. Miller

The National Aeronautics and Space Administration

NASA Technical Working Group

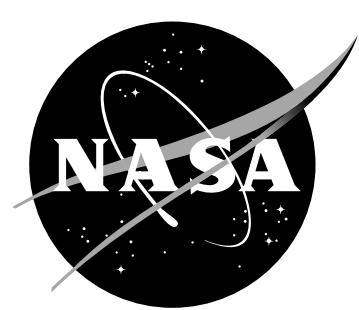
April 21st-22nd 2015

Based on Miller, S. A. E., "Toward a Nonlinear Acoustic
Analogy: Turbulence as a Source of Sound and Nonlinear
Propagation," NASA TM, 2015.

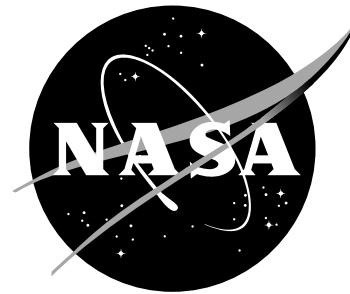


Acknowledgements

- NASA Advanced Air Vehicles Program
Commercial Supersonic Technology Project
- Brian Howerton - NASA Langley - measurements
from NASA Normal Incidence Tube
- Emily Mazur - NASA 2012 Intern - evaluated
Blackstock bridging function
- Many previous curious researchers



Introduction



Turbulence and Nonlinear Propagation

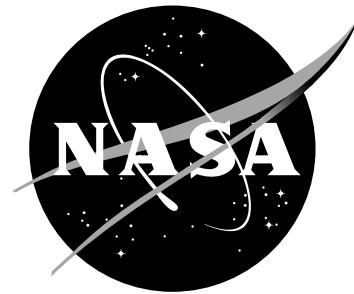
- Aerospace vehicles produce turbulence
- Sound propagates nonlinearly if turbulence is highly intense
- Intense noise is harmful to the vehicle and environment



Rocket noise has nonlinear propagation effects
NASA SMAT Test (NASA.gov)

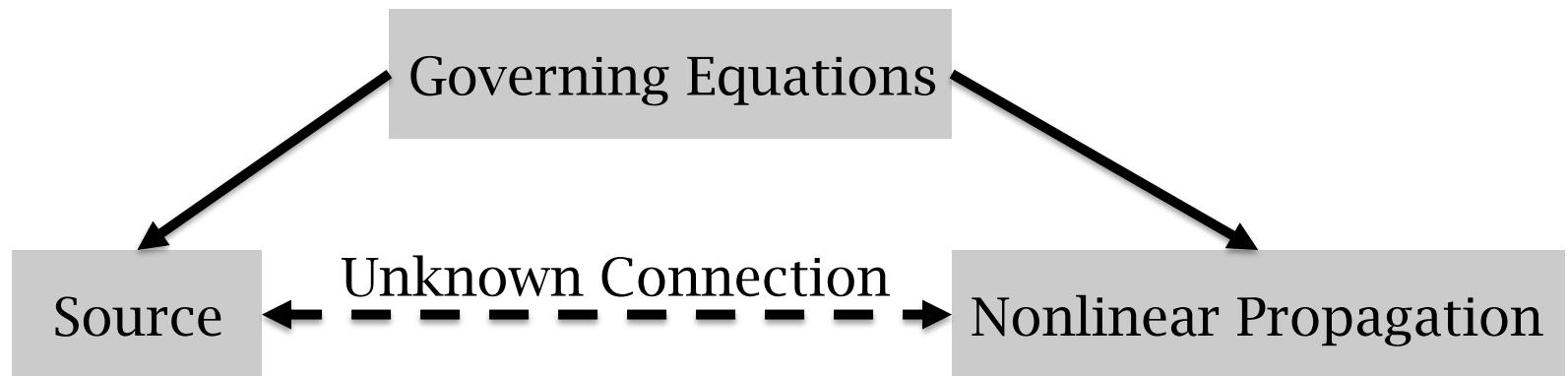


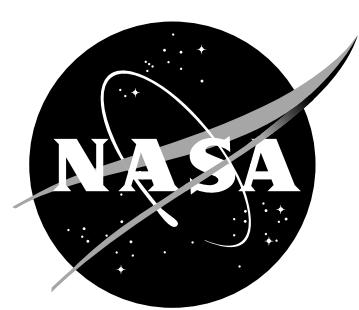
Airbreathing engine jet noise propagation effects
NASA CST Test (NASA.gov)



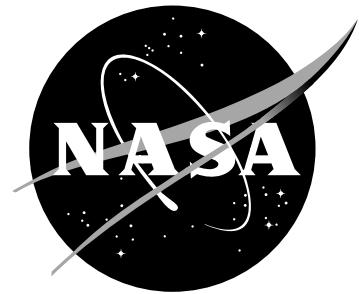
Turbulence and Nonlinear Propagation

- Understand different mathematical models of sound generation and propagation
- Relate the governing equations to sound generation and propagation
- Show a mathematical connection between sound generation (acoustic analogy) and sound propagation (Burgers' equation)





Mathematical Models



Claude-Louis Navier and George Gabriel Stokes

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_i}{\partial x_i} = 0 \quad \frac{\partial \rho u_i}{\partial t} + \frac{\partial \rho u_i u_j}{\partial x_j} = \frac{\partial \tau_{ij}}{\partial x_j}$$
$$\frac{\partial \rho e_o}{\partial t} + \frac{\partial \rho u_j e_o}{\partial x_j} = -\frac{\partial u_j p}{\partial x_j} - \frac{\partial q_j}{\partial x_j} + \frac{\partial u_i \tau_{ij}}{\partial x_j}$$



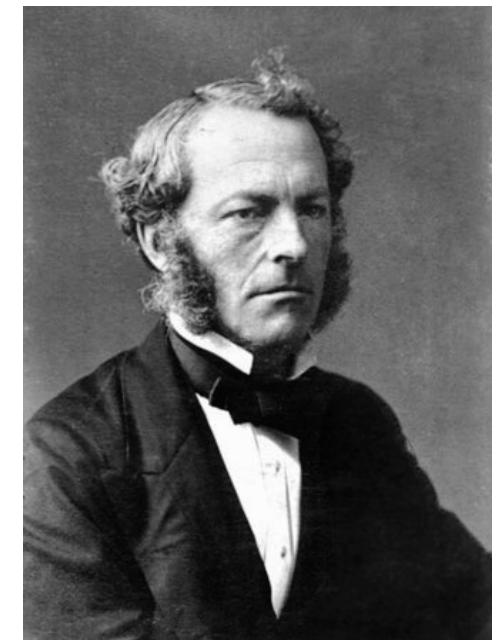
Navier

Claude-Louis Marie
Henri Navier

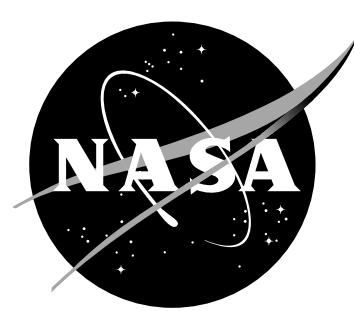
- 1735-1836
- French
- Professor at École Nationale des Ponts et Chaussées
- Known for elasticity and structural engineering

Sir George Stokes

- 1819-1903
- Irish
- Lucasian Professor
- Fluids, Optics, Chemistry
- Politics and Theology



Stokes



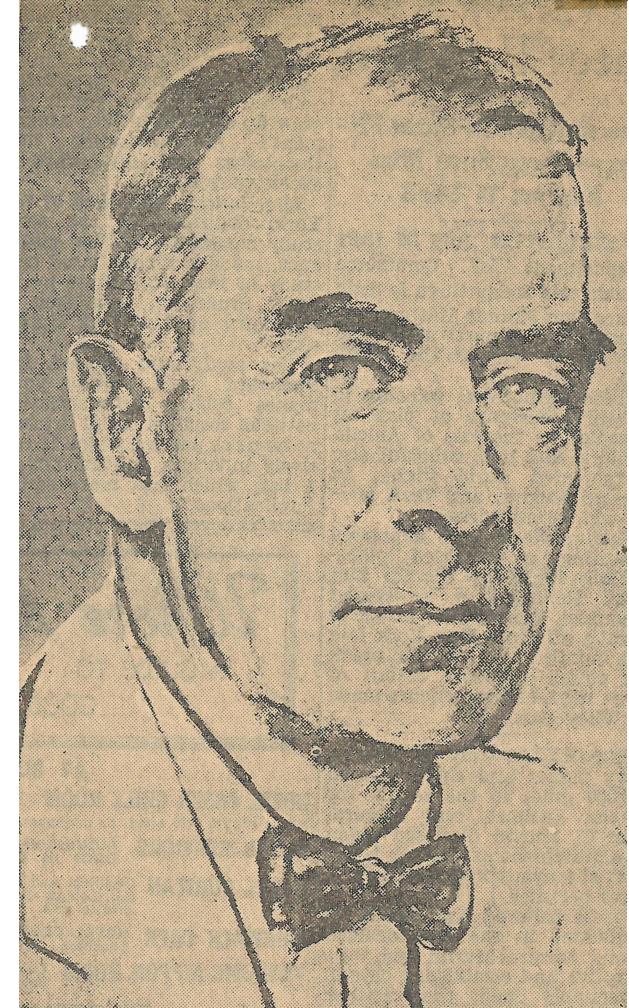
Richard D. Fay

Governing Equation (Conjecture)

$$c_\infty^2 \frac{\partial^2 y}{\partial x^2} = \frac{\partial y}{\partial x}^{\gamma+1} \left[\frac{\partial^2 y}{\partial t^2} - \frac{4\mu}{3\rho_\infty} \frac{\partial}{\partial t} \left(\frac{\partial^2 y}{\partial x^2} \right) \right]$$

- Governs shocked one-dimensional finite amplitude waves
- y is particle displacement
- Solution via assumptions
 - Periodic
 - dy / dx is Fourier series
 - Substitute and solve Fourier series

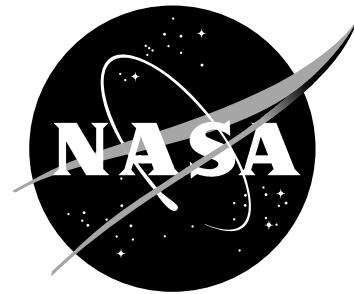
Fay, R. D., "Plane Sound Waves of Finite Amplitude,"
Journal of the Acoustical Society of America, Vol. 3, No.
9, 1931, pp. 222-241. doi:10.1121/1.1901928.



Courtesy of the MIT Electrical Engineering and Computer Science Department

Solution

$$\frac{p}{p_\infty} = \frac{32}{3} \frac{\mu\omega}{c_\infty^2 \rho_\infty} \left(\frac{\gamma}{\gamma+1} \right) \sum_{n=1}^{n=\infty} \frac{\sin n(\omega t - \omega x/c_\infty)}{\sinh n \left[\log \left[\frac{16\mu\omega}{3\rho_\infty(\gamma+1)c_\infty^2 K_{1,1}} \right] + \frac{2x\mu\omega^2}{3c_\infty^3 \rho_\infty} \right]}$$



Guido Fubini-Ghiron

Governing Equation (Conjecture)

$$\frac{\partial^2 \xi}{\partial t^2} + \frac{\partial \xi}{\partial t} \frac{\partial^2 \xi}{\partial x \partial t} = -\frac{1}{\rho} \frac{\partial p}{\partial x}$$

- Continuous non-conservative one-dimensional finite amplitude waves
- ξ is particle displacement
- Solution via Earnshaw approach
 - Write as binomial series and truncate
 - Convert to Eulerian framework and rewrite as Fourier series

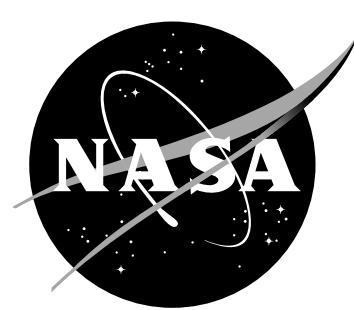
Solution

$$\frac{p}{p_\infty} = \sum_{n=1}^{\infty} \frac{2}{n\sigma} J_n[n\sigma] \sin n(\omega t - kx)$$

Fubini-Ghiron, G., “Anomalie nella Propagazione di onde Acustiche di Grande Ampiezza,” Alta Frequenza, Vol. 4, 1935, pp. 530-581.



Italian, 1879-1943, Professor of Mathematics at Princeton



David T. Blackstock

Governing Equations (Conjecture)

$$u = g(\phi) \quad \tau = \phi - (\beta c_\infty^{-2})g(\phi)$$

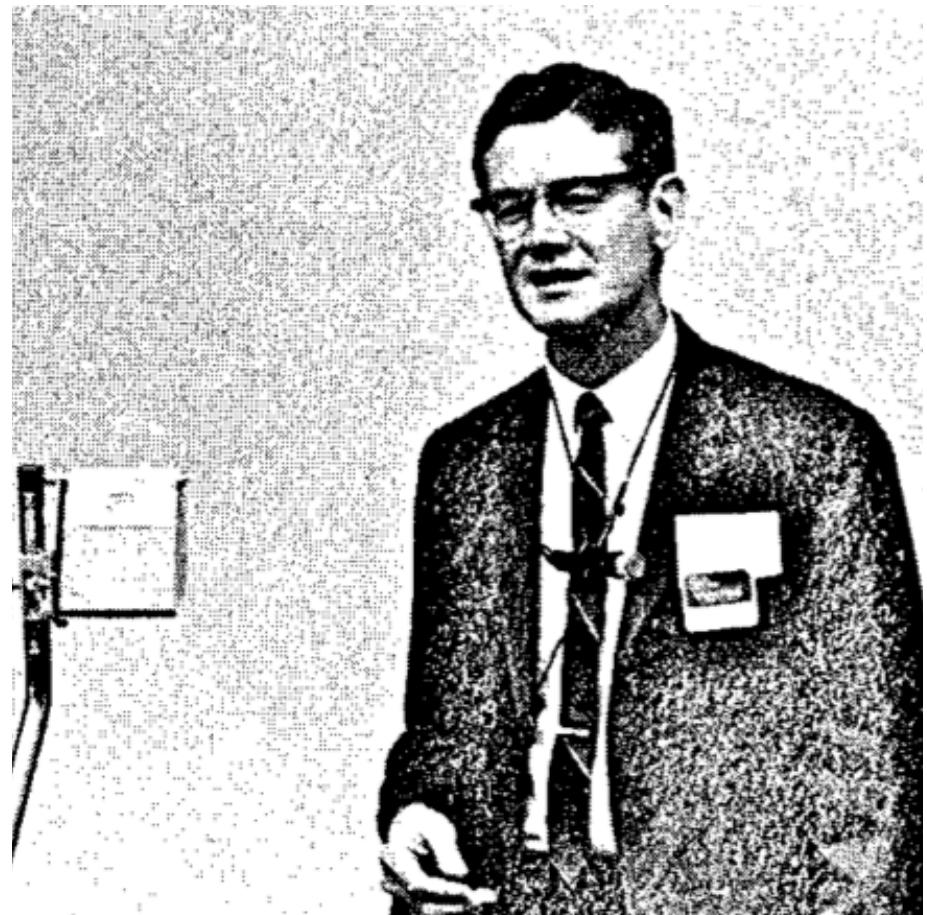
$$\frac{dt'_s}{dx} = -\frac{1}{2}\beta c_\infty^{-2}(u_a + u_b)$$

- Weak shock theory
- g is a function and ϕ is emission time
- Direct solution approach by substitution after eliminating ϕ
 - Assume boundary value problem
 - Resultant transcendental equation solved with Fourier series assumption

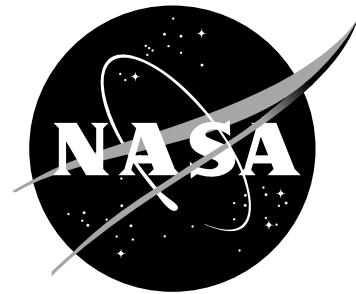
Solution

$$p(x, t) = p_o \sum_{n=1}^{\infty} B_n \sin [n\omega\tau]$$
$$B_n = \frac{2}{n(1+\sigma)} + \frac{2}{n\pi\sigma} \int_{\Phi_{sh}}^{\pi} \cos [n(\Phi - \sigma \sin \Phi)] d\Phi$$

Blackstock, D. T., "Connection Between the Fay and Fubini Solutions for Plane Sound Waves of Finite Amplitude," Journal of the Acoustical Society of America, Vol. 39, No. 6, 1965, pp. 1019-1026. doi:10.1121/1.1909986.



Blackstock, D. T., 'History of Nonlinear Acoustics and a Survey of Burgers' and Related Equations,' 1969.



M. J. Lighthill

Governing equations are Navier-Stokes

- Exactly rearrange to form a governing equation, the acoustic analogy

$$\frac{\partial^2 \rho}{\partial t^2} - c_\infty^2 \frac{\partial^2 \rho}{\partial x_i \partial x_i} = \frac{\partial^2 T_{ij}}{\partial x_i \partial x_j}$$

- Right hand side is equivalent source
- Left hand side is linear wave operator

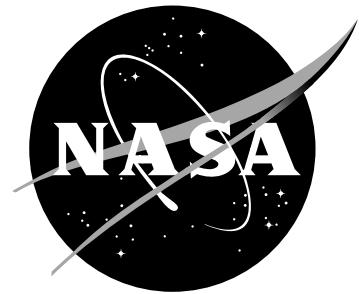
Lighthill, M. J., "On Sound Generated Aerodynamically. I. General Theory," Proc. R. Soc. Lond. A., Vol. 211, No. 1107, 1952, pp. 564–587.
doi:10.1098/rspa.1952.0060.

One solution loosely based on Ffowcs Williams

$$S(\mathbf{x}, \omega) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{r_i r_j r'_l r'_m}{c_\infty^4 r^2 r'^2} g(\mathbf{x}, \mathbf{y}, \omega) g^*(\mathbf{x}, \mathbf{y}', \omega) \frac{\partial^4}{\partial \tau^4} R_{ijlm}(\mathbf{y}, \boldsymbol{\eta}, \tau) \\ \times \exp \left[-i\omega \left(\tau + \frac{r}{c_\infty} - \frac{r'}{c_\infty} \right) \right] d\tau d\boldsymbol{\eta} d\mathbf{y}$$



English (born Paris),
1924-1998, Lucasian
Professor at Cambridge



David G. Crighton

Governing equations is Navier-Stokes

- Assume
 - u is summation of a gradient and cross-product, eliminate high order terms, flow is irrotational
 - Solutions are set of symmetry
 - $Kr \gg 1$, 'linear wavenumber'

Governing Equation (non-gen. Burgers')

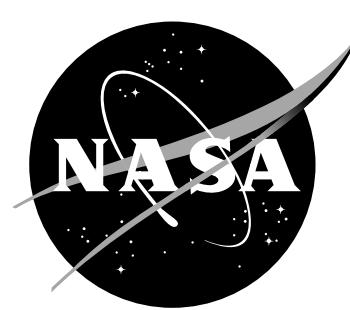
$$\frac{\partial u}{\partial t} + c_\infty \frac{\partial u}{\partial r} + \frac{\gamma + 1}{2} u \frac{\partial u}{\partial r} + \frac{jc_\infty u}{2r} = \frac{\delta}{2} \frac{\partial^2 u}{\partial r^2}$$

- Spherical, cylindrical, and planar nonlinear wave propagation

Crighton, D. G., "Model Equations of Nonlinear Acoustics,"
Annual Review of Fluid Mechanics, Vol. 11, 1979, pp. 11-33.
doi:10.1146/annurev.fl.11.010179.000303.



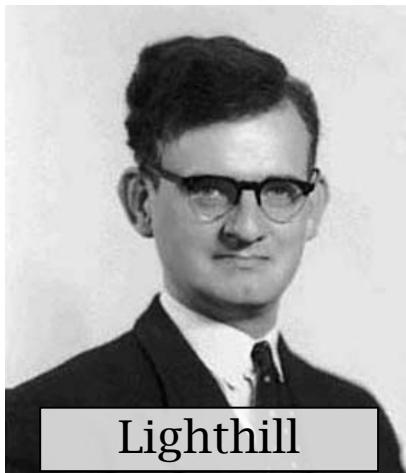
English, 1942-2000, Professor
of Applied Mathematics
Cambridge
Also Opera lover - so am I! :)



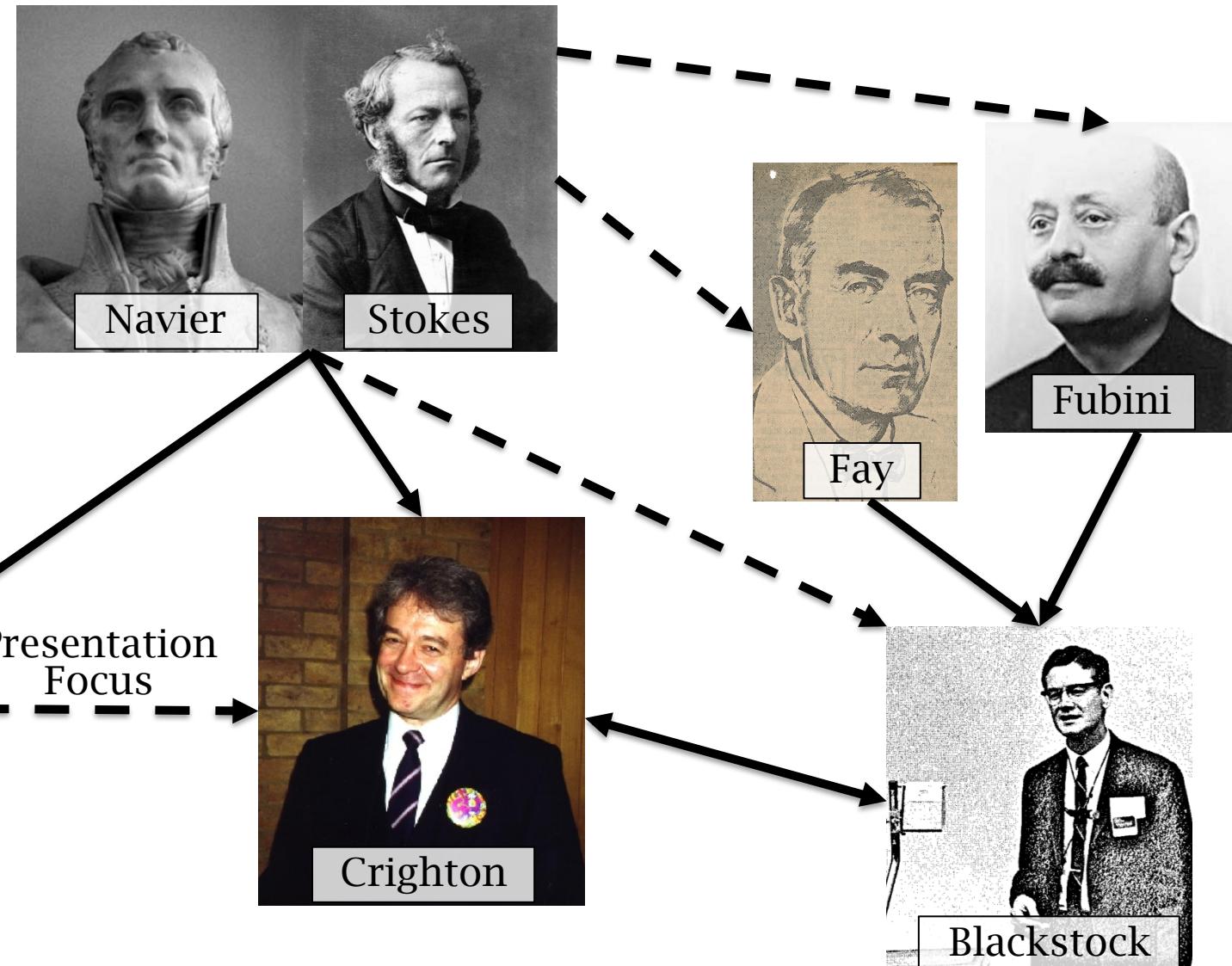
Known Derivation
and/or Known
Solution



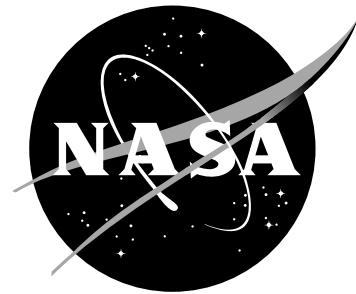
Newly Developed
Derivation
and/or Solution



Lighthill



Miller NASA TM shows the mathematical connections and solutions of ALL relations!



The Navier-Stokes Equations and the Acoustic Analogy

Governing equations are Navier-Stokes.

We now think of the Green's function as satisfying

$$\rho(\mathbf{x}, t) = \int_{-\infty}^{\infty} \dots \int_{-\infty}^{\infty} g \frac{\partial^2 T_{ij}}{\partial x_i \partial x_j} d\tau d\mathbf{y}$$

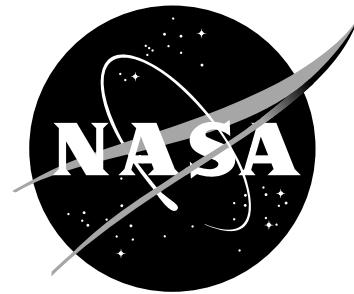
We can show using the cross-spectral acoustic analogy

$$\begin{aligned} S(\mathbf{x}, \omega) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{r_i r_j r'_l r'_m}{c_{\infty}^4 r^2 r'^2} g(\mathbf{x}, \mathbf{y}, \omega) g^*(\mathbf{x}, \mathbf{y}', \omega) \frac{\partial^4}{\partial \tau^4} R_{ijlm}(\mathbf{y}, \boldsymbol{\eta}, \tau) \\ \times \exp \left[-i\omega \left(\tau + \frac{r}{c_{\infty}} - \frac{r'}{c_{\infty}} \right) \right] d\tau d\boldsymbol{\eta} d\mathbf{y} \end{aligned}$$

A statistical source model for sound generation (altered from Miller) is

$$\begin{aligned} \frac{\partial^4}{\partial \tau^4} R_{ijlm}(\mathbf{y}, \boldsymbol{\eta}, \tau) = \frac{4A_{ijlm}\bar{u}^4}{\pi^{1/2} l_s^8} (3l_s^4 - 12l_s^2(\xi - \bar{u}\tau)^2 + 4(\xi - \bar{u}\tau)^4) \\ \times \exp \left[\frac{-|\xi|}{\bar{u}\tau_s} \right] \exp \left[\frac{-(\xi - \bar{u}\tau)^2}{l_s^2} \right] \exp \left[\frac{-\eta^2}{l_{sy}^2} \right] \exp \left[\frac{-\zeta^2}{l_{sz}^2} \right] \end{aligned}$$

Miller, S. A. E., "Prediction of Near-Field Jet Cross Spectra," AIAA Journal, 2015. doi:10.2514/1.J053614.



The Navier-Stokes Equations and the Acoustic Analogy

Using the source model, assuming that the observer is in the far-field, simplifying, and carefully rearranging yields

$$S(\mathbf{x}, \omega) = \frac{\pi \omega^4}{c_\infty^4} g(\mathbf{x}, \omega) g^*(\mathbf{x}, \omega) \int_{-\infty}^{\infty} A_{ijlm} \frac{r_i r_j r_l r_m}{r^4} \frac{l_s l_{sy} l_{sz}}{\bar{u}} \exp \left[\frac{-l_s^2 \omega^2}{4\bar{u}^2} \right]$$

Green's function

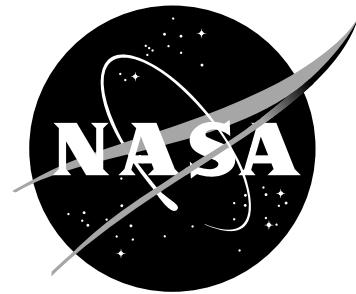
Source Spectrum

$$\times \int_{-\infty}^{\infty} \exp \left[\frac{-i\xi\omega}{\bar{u}} \right] \exp \left[\frac{-|\xi|}{\bar{u}\tau_s} \right] d\xi dy_1$$

Selective far-field assumption

- Source remains a volumetric integral
- Propagation approximated from a point within source volume

Need to find what $g g^*$ is to capture nonlinear propagation effects



The Navier-Stokes Equations and a Burgers' Equation

The Navier-Stokes equations

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_i}{\partial x_i} = 0 \quad \text{and} \quad \frac{\partial \rho u_i}{\partial t} + \frac{\partial \rho u_i u_j}{\partial x_j} = \frac{\partial \tau_{ij}}{\partial x_j}$$

Following Crighton then finding a more compact form governing pressure

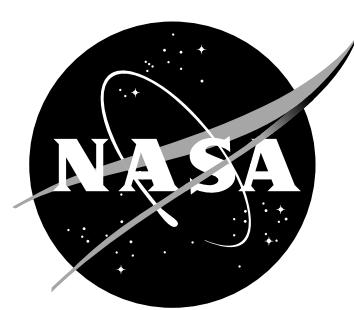
$$\frac{\partial p}{\partial x} + m \frac{p}{r} - \epsilon p \frac{\partial p}{\partial \tau} = \frac{\delta}{2c_\infty^3} \frac{\partial^2 p}{\partial \tau^2}$$

Select analytical solutions exist - eg: Blackstock, Fay, and Fubini

Seek a numerical solution in the frequency domain (as shown by Saxena)

$$\frac{\partial \tilde{p}}{\partial r} + m \frac{\tilde{p}}{r} + (\alpha + i\beta) \tilde{p} = \frac{i\omega\epsilon}{2} \tilde{q}$$

Pseudo-spectral numerical method marches solution in space from prescribed boundary condition (same BC as Blackstock)



The Connection Between the Acoustic Analogy and Generalized Burgers' Equation

Conjecture: Given the solution of

$$\frac{\partial \tilde{p}}{\partial r} + m \frac{\tilde{p}}{r} + (\alpha + i\beta) \tilde{p} = \frac{i\omega\epsilon}{2} \tilde{q}$$

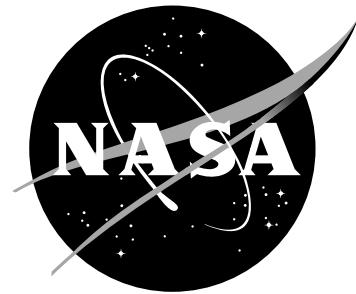
subject to the boundary condition of a source spectrum of the acoustic analogy and $x \gg D$ then

$$g(\mathbf{x}, \omega)g^*(\mathbf{x}, \omega) \approx \tilde{p}(\mathbf{x}, \omega)\tilde{p}^*(\mathbf{x}, \omega)$$

within the acoustic analogy. As $\lim \tilde{p} \rightarrow \epsilon$

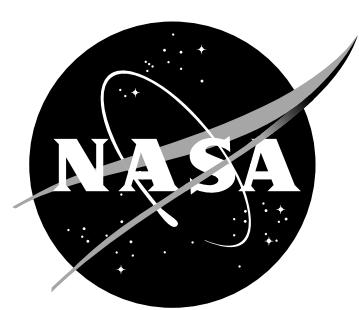
$$g(\mathbf{x}, \omega)g^*(\mathbf{x}, \omega) = \tilde{p}(\mathbf{x}, \omega)\tilde{p}^*(\mathbf{x}, \omega)$$

for the traditional approach only.

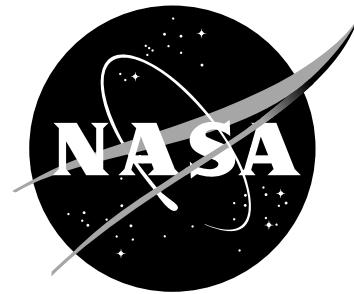


Acoustic Analogy and Burgers' Equation

- Approximation of gg^* is obtained from solution of generalized Burgers' equation
- Boundary condition (at $r = 0$) of generalized Burgers' equation is broadband source spectrum
- Source spectrum at low intensities results in predictions that are equivalent to those produced by traditional acoustic analogies
- Source spectrum at high intensity causes nonlinear terms within generalized Burgers' equation to be dominant
- Characteristics of nonlinear propagation are apparent in predicted jet mixing noise spectrum.

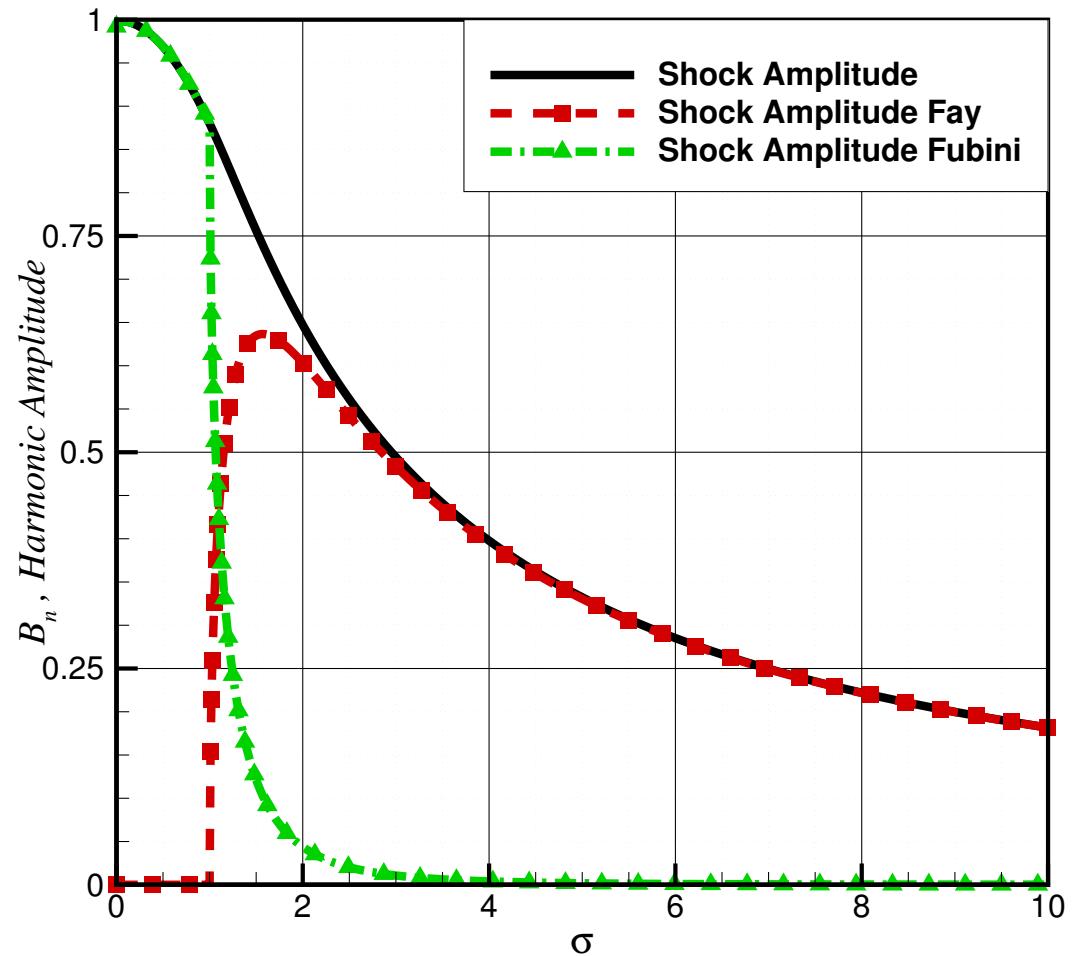


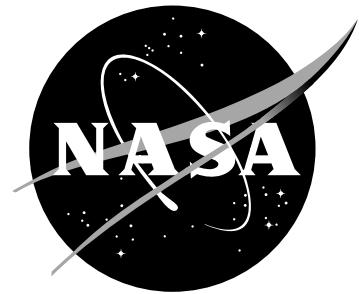
Results



Examination of Blackstock, Fay, and Fubini

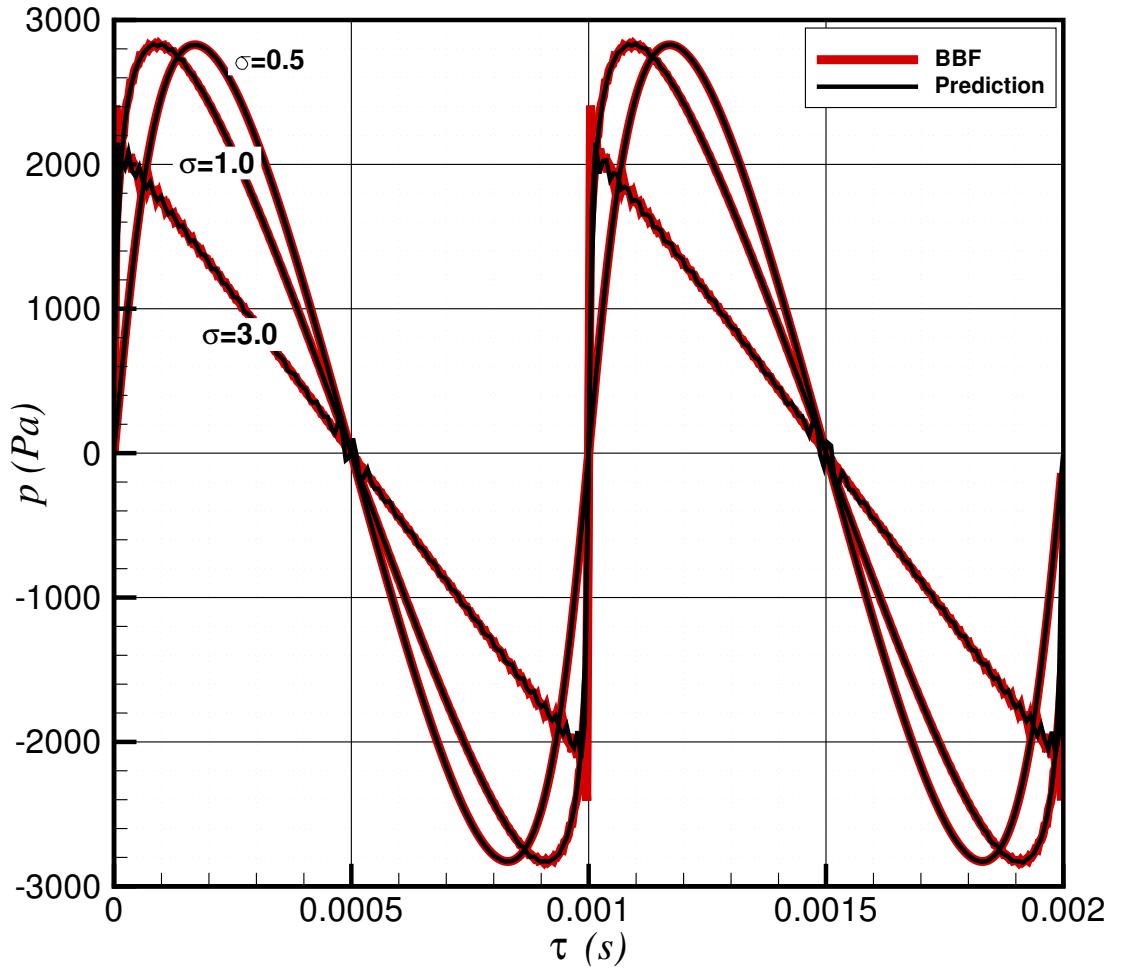
- Almost exact solutions of generalized Burgers' equation
- Source planar sin wave at 160dB and 1000Hz
- Regions of validity

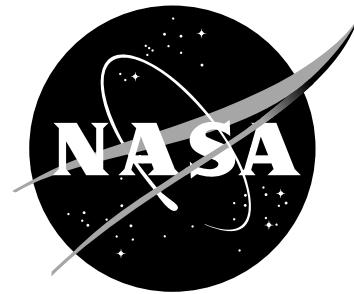




Numerical Solver of Generalized Burgers' Equation and Blackstock Bridging Function

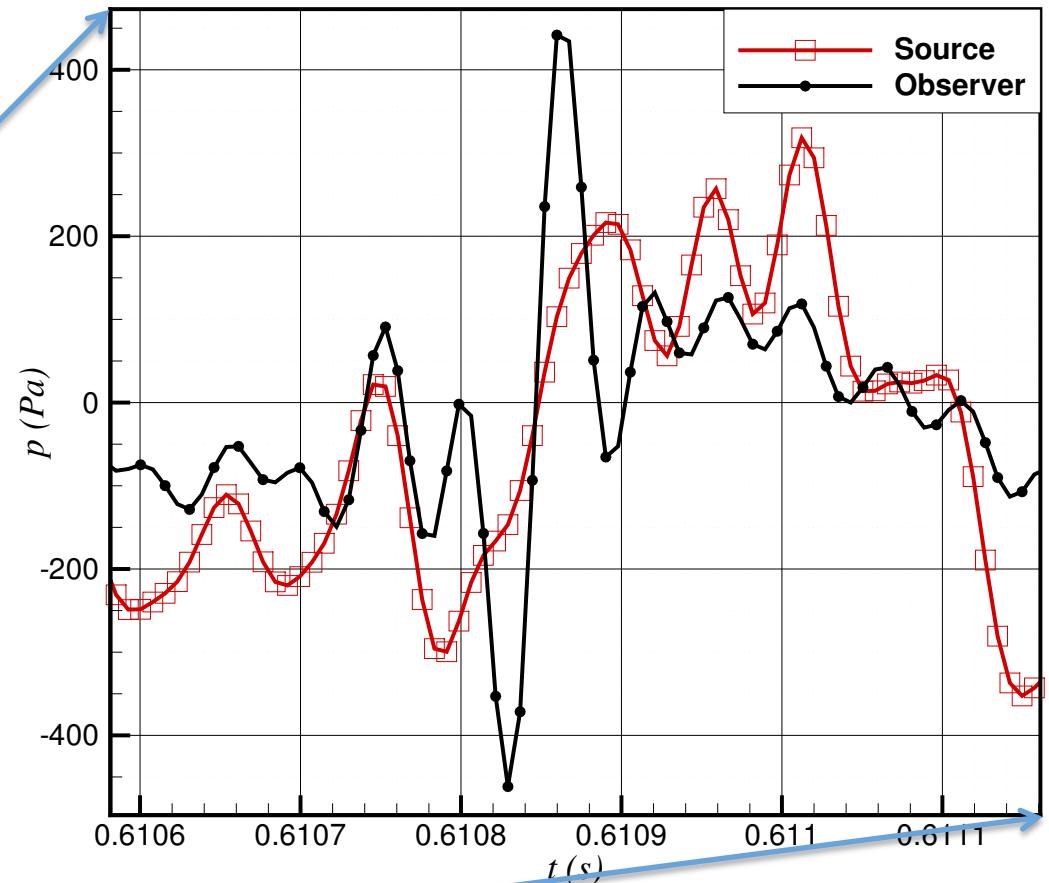
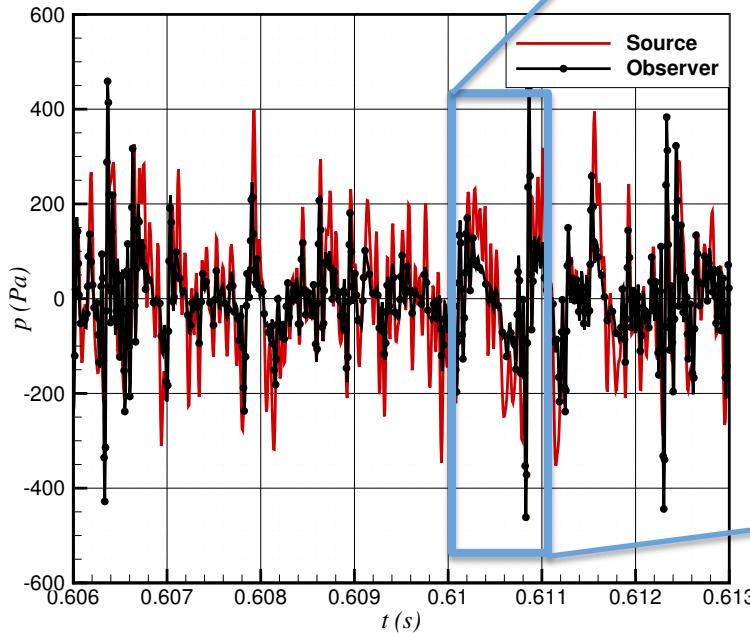
- Comparison at three observer positions
- Numerical solver agrees with analytic result
- Source planar sin wave at 160dB and 1000Hz
- Gibb's phenomenon present

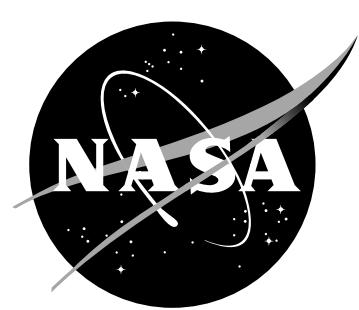




Propagation of a Broadband Signal

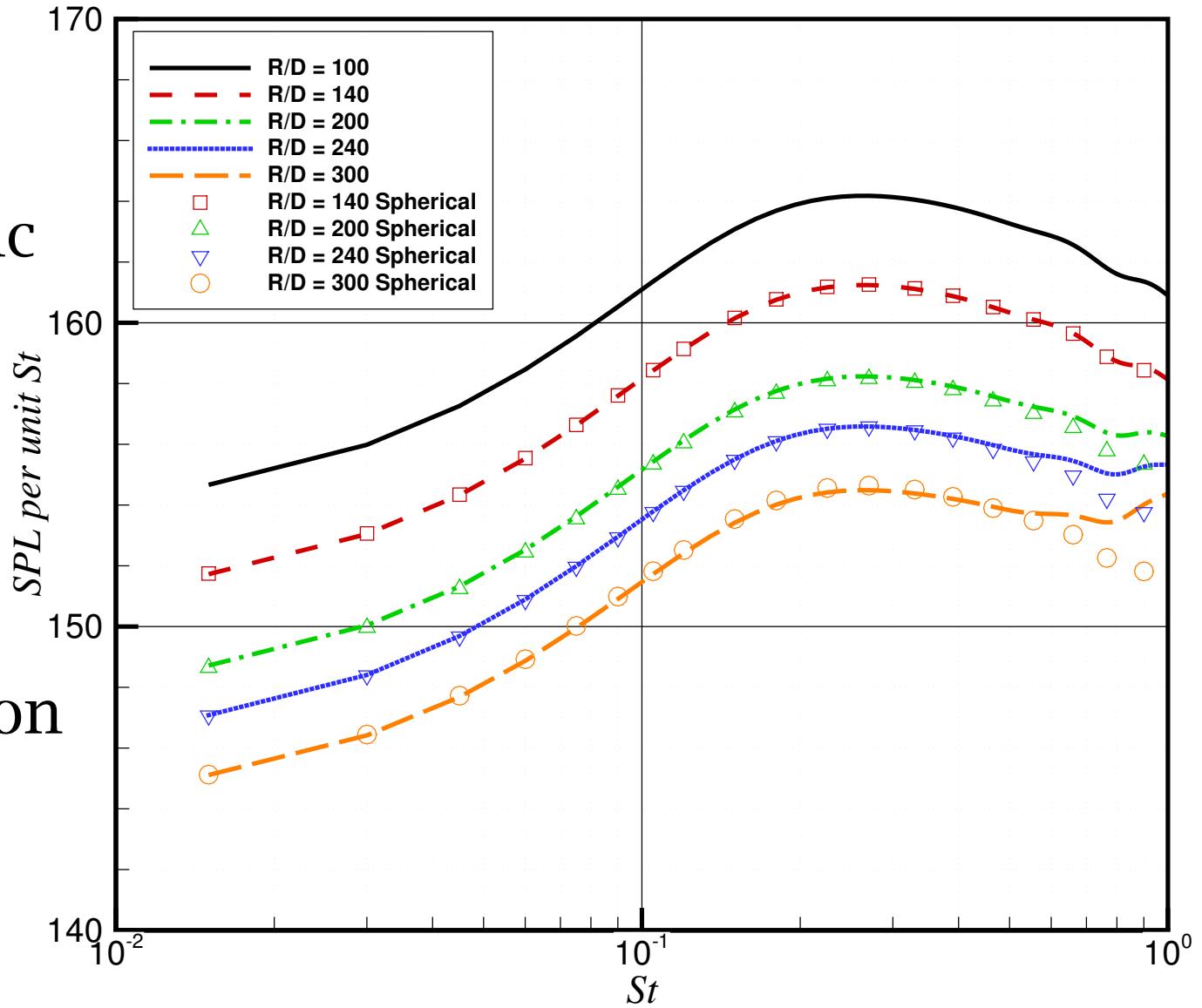
- Shocked observer waveform due to wave coalescence
- Discontinuities not present in source signal
- Not observed in linear acoustics
- Jet $M_j = 1.86$
- Jet TTR = 3.20
- Sideline direction

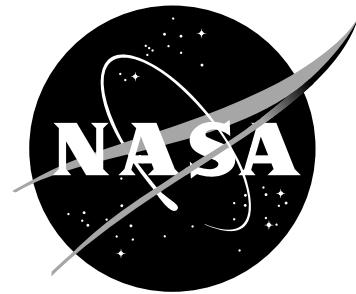




Example Jet Noise Prediction Directly Incorporating Nonlinear Propagation

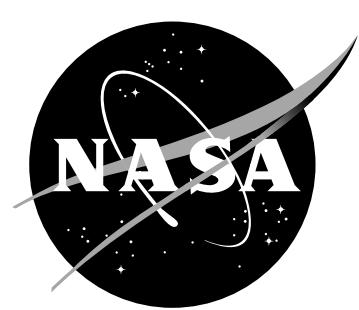
- Unified Acoustic Analogy with Nonlinear Propagation
- Jet $M_j = 1.86$
- Jet TTR = 3.20
- Sideline direction



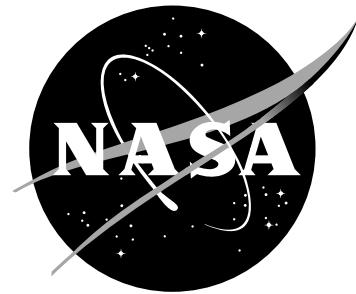


Summary and Conclusion

- Showed connection between Navier-Stokes equations, generalized Burgers' equation (sound propagation), and Acoustic Analogy (sound source)
- Nonlinear propagation taken into account directly from source to observer
- A single equation contains sound source and nonlinear propagation from turbulence
- Evaluated select equations to demonstrate relevant physics

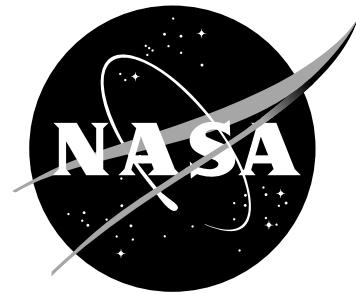


Questions



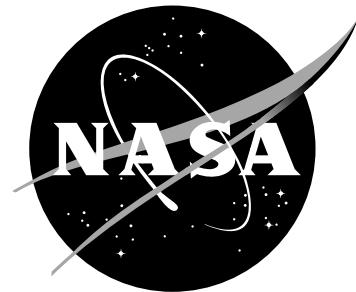
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